PRELIMINARY DRAINAGE ANALYSIS

FOR

THE OAK COTTAGE OF SANTA BARBARA 1820, 1822, & 1826 DE LA VINA STREET SANTA BARBARA, CA

Prepared: August 4, 2010

By:

InsiteCivil, Inc.
615 S. Main Street, Suite D
Templeton, CA 93465

For:

Mark and Valerie Maldonado



I. PURPOSE AND SCOPE

The purpose of this report is to provide a preliminary drainage analysis for the proposed memory care facility located at 1820, 1822, and 1826 De La Vina Street in the City of Santa Barbara, CA. This report will address pre- and post development storm water peak discharge rates, volume reduction and storm water quality as required by the City of Santa Barbara's Storm Water Management Program.

II. EXISTING CONDITIONS

The site consists of three separate assessor's parcels (APN 027-020-022, 023, and 024) with a combined site area of approximately 28,350 square feet. The site is bounded by De La Vina Street to the west and existing residences to the north, south and east. Site topography slopes downhill gradually in a south westerly direction then drops approximately six feet within approximately 12 feet to De La Vina Street. The site is currently developed with six buildings including three residences, two garages, and one shed. Currently, site storm water runoff drains overland to the De La Vina Street gutter (Refer to Exhibit 1).

Based upon the United States Department of Agriculture (USDA) Soil Survey Map for this site, the soils are classified as Hydrologic Soils Group D and are defined as Milpitas-Positas Fine Sandy Loams.

Percolation tests performed by Coast Valley Testing, Inc. on November 5, 2008 yielded an infiltration rate of 1.5 inches per hour (40 min. /in.) (Refer to Exhibit 2).

III. PROPOSED CONDITIONS

The project consists of a proposal to demolish the existing buildings and constructing a two-story 40-unit residential care facility for the elderly with a 9,090 square foot building footprint and 5,590 square feet of covered parking. A new permeable driveway will be constructed along with landscaped areas serving as bioretention areas and filter strips.

IV. METHODOLOGY

The development area was subdivided into watershed areas contributing to each drainage facility (Refer to Exhibit 3).

Hydrology and detention calculations for the site are based on the Santa Barbara County Urban Hydrograph Method (SBUH) for the 25-year storm utilizing the HydroCAD Stormwater Modeling System program developed by HydroCAD Software Solutions LLC.

Infiltration and bioretention sizing calculations are based on the simple sizing method in accordance with the City of Santa Barbara DRAFT – Post Construction Stormwater BMPs, Technical Guidance Manual.

V. HYDROLOGIC RESULTS

Existing 25-Year Hydrological Results

The 25-year pre-development peak flow from the project site was calculated to be 1.74 cubic feet per second (Refer to Worksheet No. 1).

Proposed 25-Year Hydrological Results

The post-development 25-year flow from the project site was calculated to be 1.75 cubic feet per second (Refer to Worksheet No. 2).

NODE	25-YR PEAK DISCHARGE (CFS)
Pond 1P	0.75
Pond 2P	0.33
Subcatchment 3S	0.19
Subcatchment 4S	0.25
Subcatchment 5S	0.23
TOTAL	1.75

Two 30-inch diameter underground pipes (Pond 1P and Pond 2P) are proposed as detention facilities to accommodate the runoff volume from the 25-year storm while releasing a peak flow rate that does not exceed the existing 25-year peak flow rate in accordance with the City of Santa Barbara Storm Water Management Program and the State NPDES General Permit for Storm Water Discharges (Refer to Worksheet No. 2).

VI. STORM WATER QUALITY AND VOLUME REDUCTION

The runoff volume from the proposed impervious areas resulting from a one-inch storm will be treated by filtering through three bioretention areas. Volume reduction is also accomplished through infiltration into the subsurface soils below the bioretention areas. Calculations demonstrate that the surface areas of the proposed bioretention areas exceed the minimum infiltration requirements (Refer to Worksheet No. 3).

VII. CONCLUSIONS

A. Maintaining or Reducing Peak Discharge Rate

The proposed project mitigates increased peak runoff by incorporating underground detention pipes that accommodate the runoff volume from the 25-year storm while releasing a peak flow rate that does not exceed the existing 25-year peak flow rate.

B. Runoff Volume Reduction

Runoff volume reduction is achieved with bioretention areas designed to capture and infiltrate the runoff from the project site for a one-inch storm over a 24-hour period. The results indicate that the area of bioretention provided exceeds the minimum requirements.

C. Storm Water Quality Requirements

Storm water quality requirements are met with landscaped areas serving as bioretention areas, landscaped filter strips, permeable pavers, and trench drains fitted with filters to treat runoff resulting from a one-inch storm prior to discharging into the public drainage system.

D. Storm Drainage Conveyance Facilities

Thru curb drains will provide for positive drainage of runoff, which does not infiltrate into the subsurface soils, onto the existing public street gutters. These proposed thru-curb drains and other pipe culverts will be sized to convey the peak flow from a 25-year storm. Finished grades will be designed to allow for overland release of peak flows resulting from the 100-year storm event to the public streets.

These calculations are based on preliminary plans. Final design may result in modifications to the proposed drainage facilities as required to accommodate the approved site plan and the City's storm water runoff requirements.

VIII. Technical Appendix of Supporting Documentation for Calculations

Exhibits

- 1 Existing Site Conditions
- 2 Percolation Tests by Coast Valley Testing
- 3 Site Drainage Area Map

Worksheets

- 1 HydroCAD Summary Report Existing Runoff Calculations
- 2 HydroCAD Summary Reports Proposed Runoff Calculations
- 3 Design Infiltration and Bioretention Sizing Calculations

EXHIBIT #1

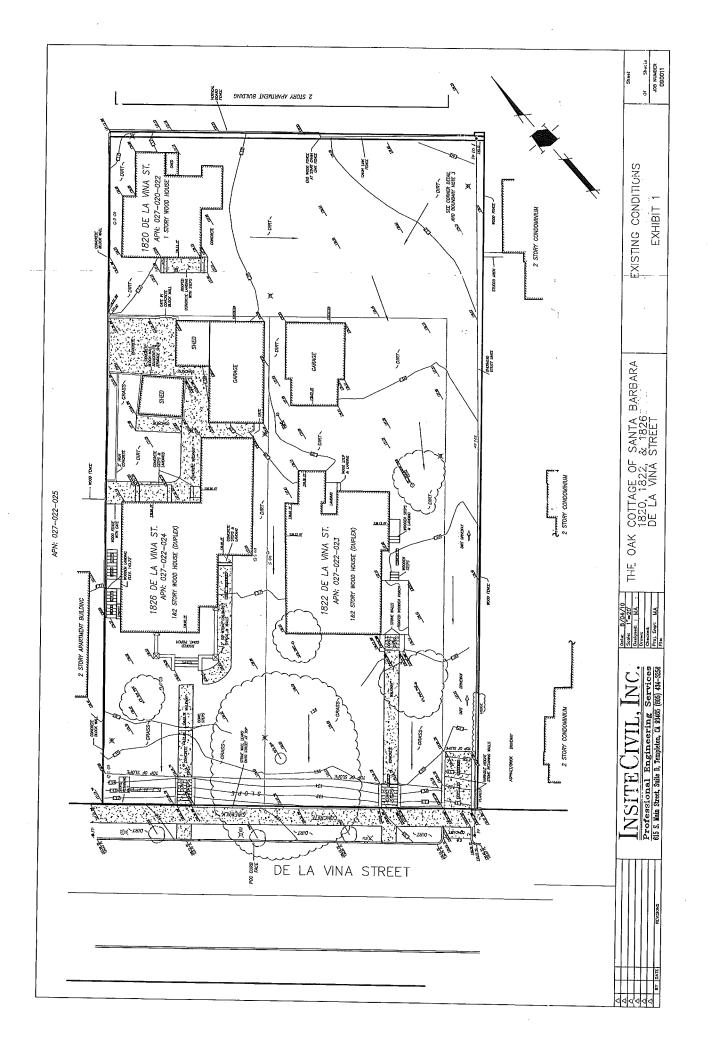


EXHIBIT #2

Coast-Valley
Testing, Tue, November 5, 2008

Page 1

Order Number: 51398

Reference Number: 08-6377

Mark Maldonado P.O. Box 3007 Santa Barbara, CA 93130 + 3007

SUBJECT: Performance Tests 1822 & 1826 De La Vina Street Santa Barbara, California

Dear Sir:

In accordance with your request this office performed percolation testing at the subject site in order to determine the suitability of subsurface soils to accept surface water for the design of permeable driveways and/or bio-swales. The tests were performed in 12 inch diameter, pre-saturated borings, using a 6 inch water head. The borings were drilled to depths of 8.0 to 10.0 feet below existing grade In addition, a six inch diameter boring was drilled to insure no free groundwater or impervious bedrock is located within 10.0 vertical feet of the proposed permeable driveway or bio-swale. The boring and percolation tests locations are shown on Appendix #1. The results are as follows:

TEST #	DEPTH	PERCOLATION RATE
		Min/In
Commission of the second secon	10.0	.4()
1	7. 50. 8.1%	
	0.5	3.6
	0,8	41)

CC: Mark Maldonado Lisa Plowman

> Respectivity. Coast Valley Testing. Inc.

Timothy J. Dolan. Presidens RCE \$3758 Expires 06-30-2010

TJD/cp

360 South Fatroism Avenue Suite A. Goleta, Palifornia 93117

Goleta Office (805) 964-3509 Los Otivos Office (805) 688-3577

- Fax (805) 969-9897

DE LA VINA SILEET Appendix # 1 Industry.

APPOXIMATE GORING LOCATIONS NO SCALE

1

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Simon S

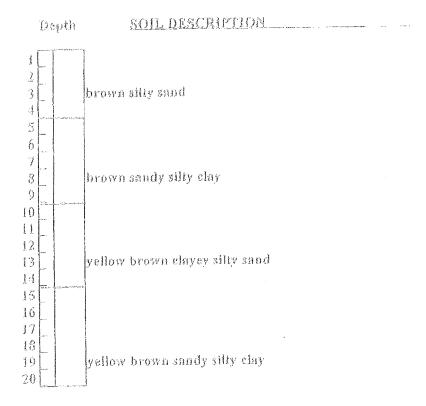
Page 3

Order Namber: 51398

Reference Number, 08-6377

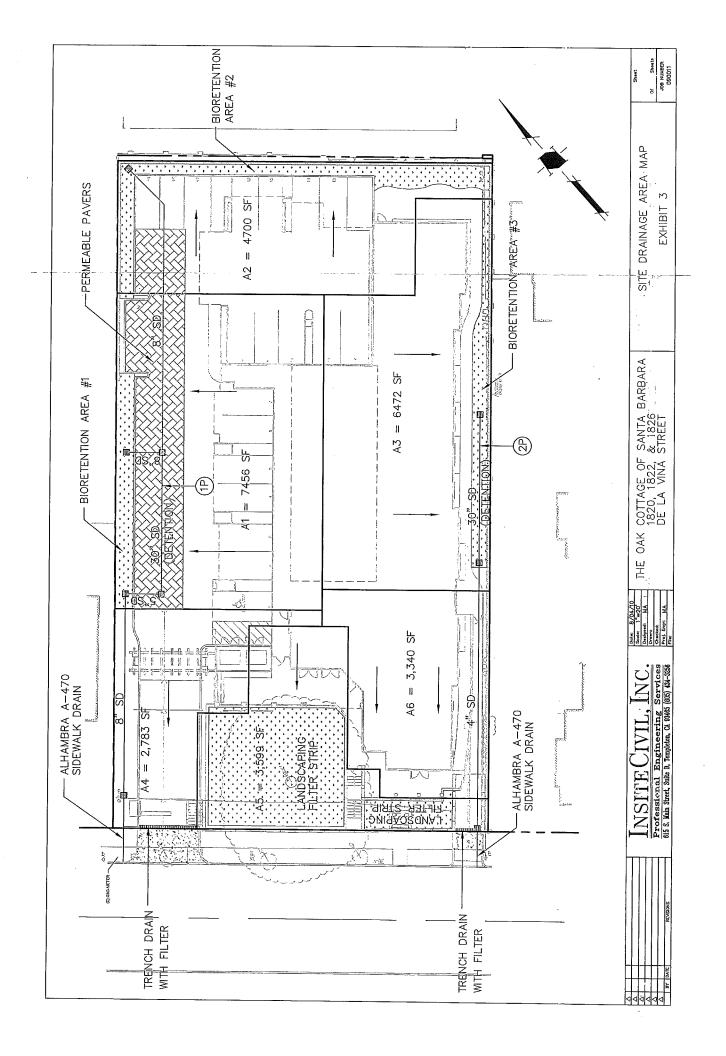
BORING LOG

Boring # 1



No bedrock No ground water @ -20.0 fee!

EXHIBIT #3



WORKSHEET #1

Printed 8/4/2010 Page 1

Summary for Subcatchment 1S: Existing Site Runoff

Runoff

=

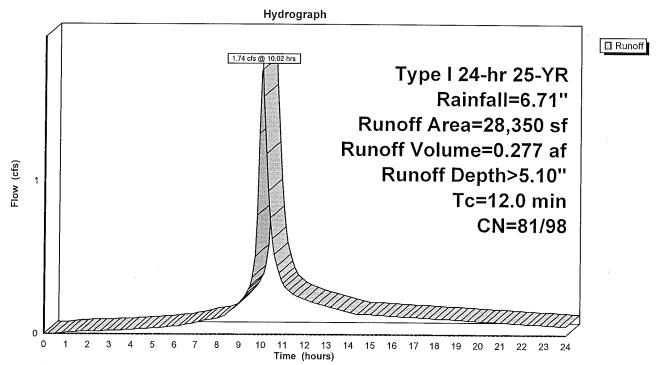
1.74 cfs @ 10.02 hrs, Volume=

0.277 af, Depth> 5.10"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

		rea (sf)	CN	Description		
		28,350	86	1/3 acre lot	s, 30% imp	p, HSG D
		19,845 8,505	81 98	Pervious Ar Impervious		
_	Tc (min)	Length (feet)	Slop (ft/fi		Capacity (cfs)	Description
	12.0					Direct Entry

Subcatchment 1S: Existing Site Runoff



WORKSHEET #2

090011_Proposed Conditions

Type I 24-hr 25-YR Rainfall=6.71" Printed 8/4/2010

Page 1

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Time span=0.00-24.00 hrs, dt=0.10 hrs, 241 points
Runoff by SBUH method, Split Pervious/Imperv.
Reach routing by Stor-Ind method

Subcatchment1S: A1 & A2 Runoff Area=12,156 sf 72.00% Impervious Runoff Depth>5.88"

Tc=12.0 min CN=80/98 Runoff=0.83 cfs 5,958 cf

Subcatchment2S: A3 Runoff Area=6,472 sf 72.00% Impervious Runoff Depth>5.88"

Tc=12.0 min CN=80/98 Runoff=0.44 cfs 3,172 cf

Subcatchment3S: A4 Runoff Area=2,783 sf 72.00% Impervious Runoff Depth>5.88"

Tc=12.0 min CN=80/98 Runoff=0.19 cfs 1,364 cf

Subcatchment4S: A5 Runoff Area=3,599 sf 72.00% Impervious Runoff Depth>5.88"

Tc=12.0 min CN=80/98 Runoff=0.25 cfs 1,764 cf

Subcatchment5S: A6 Runoff Area=3,340 sf 72.00% Impervious Runoff Depth>5.88"

Tc=12.0 min CN=80/98 Runoff=0.23 cfs 1,637 cf

Pond 1P: 30" PIPE Peak Elev=131.16' Storage=0.004 af Inflow=0.83 cfs 5,958 cf

5.0" x 12.0' Culvert Outflow=0.75 cfs 5,955 cf

Pond 2P: 30" PIPE Peak Elev=132.00' Storage=0.003 af Inflow=0.44 cfs 3,172 cf

4.0" x 45.0' Culvert Outflow=0.33 cfs 3,171 cf

Total Runoff Area = 28,350 sf Runoff Volume = 13,895 cf Average Runoff Depth = 5.88" 28.00% Pervious = 7,938 sf 72.00% Impervious = 20,412 sf

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Page 2

Summary for Subcatchment 1S: A1 & A2

Runoff

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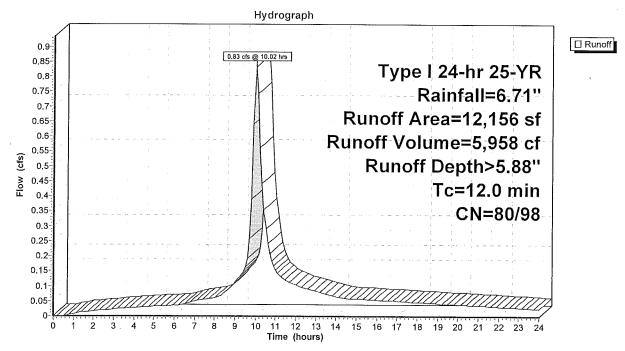
0.83 cfs @ 10.02 hrs, Volume=

5,958 cf, Depth> 5.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

A	rea (sf)	CN	Description		
	12,156	93	Urban indu	strial, 72%	imp, HSG D
	3,404	80	Pervious A	rea	
	8,752	98	Impervious	Area	
Тс	Longth	Clan	a Volgoity	Canacity	Description
	Length	Slop	•		Description
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)	
12.0					Direct Entry,

Subcatchment 1S: A1 & A2



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Page 3

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Summary for Subcatchment 2S: A3

Runoff

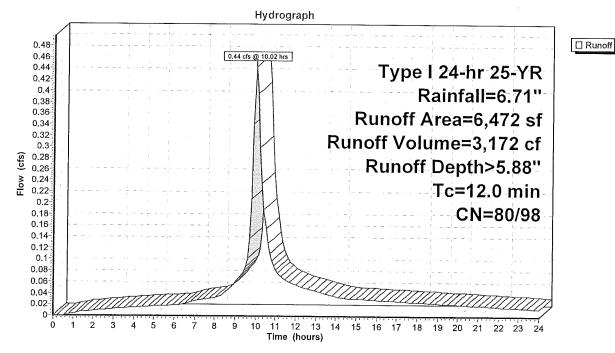
0.44 cfs @ 10.02 hrs, Volume=

3,172 cf, Depth> 5.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

A	rea (sf)	CN	Description			
	6,472	93	Urban indu	strial, 72%	imp, HSG D	
	1,812 4,660	80 98	Pervious Ar Impervious			,
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)		
12.0					Direct Entry.	

Subcatchment 2S: A3



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Page 4

Summary for Subcatchment 3S: A4

Runoff

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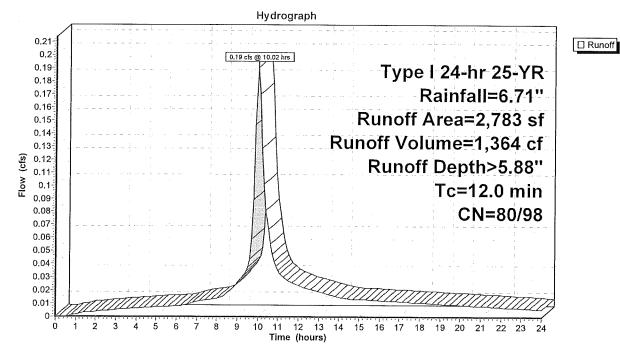
0.19 cfs @ 10.02 hrs, Volume=

1,364 cf, Depth> 5.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

A	rea (sf)	CN	Description		
	2,783	93	Urban indu	strial, 72%	imp, HSG D
	779 2,004	80 98	Pervious Ai Impervious		
Tc (min)	Length (feet)	Slop (ft/f	•	Capacity (cfs)	Description
12.0					Direct Entry.

Subcatchment 3S: A4



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Summary for Subcatchment 4S: A5

Runoff

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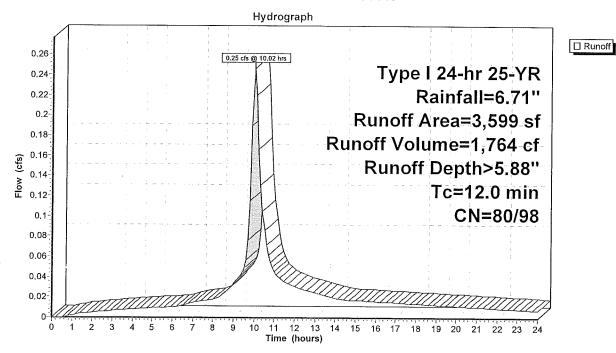
0.25 cfs @ 10.02 hrs, Volume=

1,764 cf, Depth> 5.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

A	rea (sf)	CN	Description		
	3,599	93	Urban indu	strial, 72%	imp, HSG D
	1,008 2,591	80 98	Pervious Ar Impervious		
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description
12.0					Direct Entry.

Subcatchment 4S: A5



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Page 6

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Summary for Subcatchment 5S: A6

Runoff

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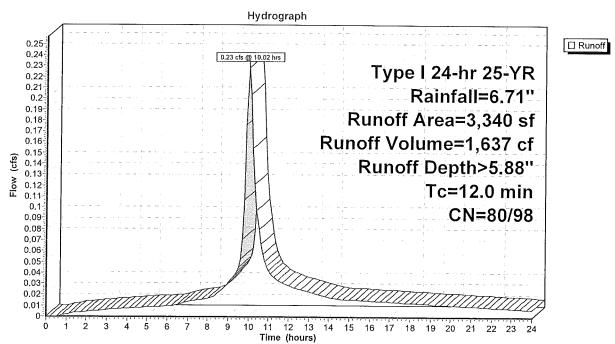
0.23 cfs @ 10.02 hrs, Volume=

1,637 cf, Depth> 5.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Type I 24-hr 25-YR Rainfall=6.71"

	Α	rea (sf)	CN	Description		
		3,340	93	Urban indu	strial, 72%	6 imp, HSG D
		935 2,405	80 98	Pervious Ai Impervious		
_	Tc (min)	Length (feet)	Slop (ft/ft	,	Capacity (cfs)	•
	12.0					Direct Entry

Subcatchment 5S: A6



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Page 7

Summary for Pond 1P: 30" PIPE

Inflow Area = 12,156 sf, 72.00% Impervious, Inflow Depth > 5.88" for 25-YR event

Inflow 0.83 cfs @ 10.02 hrs, Volume= 5,958 cf

Outflow 0.75 cfs @ 10.11 hrs, Volume= 5,955 cf, Atten= 11%, Lag= 5.2 min

Primary 0.75 cfs @ 10.11 hrs, Volume= 5,955 cf

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Peak Elev= 131.16' @ 10.10 hrs Surf.Area= 0.003 ac Storage= 0.004 af

Plug-Flow detention time= 2.1 min calculated for 5,930 cf (100% of inflow)

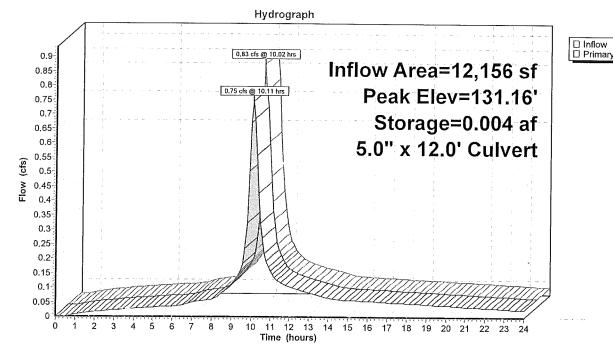
Center-of-Mass det. time= 1.7 min (716.0 - 714.3)

Volume Invert Avail.Storage Storage Description 0.005 af 30.0"D x 48.00'L Horizontal Cylinder S= 0.0010 '/' #1 129.55' Device Routing Invert Outlet Devices

#1 Primary 129.55' 5.0" x 12.0' long Culvert CPP, square edge headwall, Ke= 0.500 Outlet Invert= 129.49' S= 0.0050 '/' Cc= 0.900 n= 0.013

Primary OutFlow Max=0.74 cfs @ 10.11 hrs HW=131.15' (Free Discharge) -1=Culvert (Barrel Controls 0.74 cfs @ 5.44 fps)

Pond 1P: 30" PIPE



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Page 8

Summary for Pond 2P: 30" PIPE

Inflow Area = 6,472 sf, 72.00% Impervious, Inflow Depth > 5.88" for 25-YR event

Inflow = 0.44 cfs @ 10.02 hrs, Volume= 3,172 cf

Outflow = 0.33 cfs @ 10.18 hrs, Volume= 3,171 cf, Atten= 27%, Lag= 9.9 min

Primary = 0.33 cfs @ 10.18 hrs, Volume= 3,171 cf

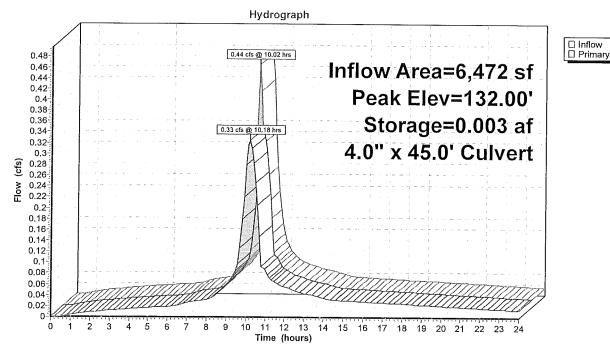
Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.10 hrs Peak Elev= 132.00' @ 10.18 hrs Surf.Area= 0.003 ac Storage= 0.003 af

Plug-Flow detention time= 2.7 min calculated for 3,171 cf (100% of inflow) Center-of-Mass det. time= 2.4 min (716.6 - 714.3)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	130.47'	0.005 af	30.0"D x 48.00'L Horizontal Cylinder S= 0.0010 '/'
Device	Routing	Invert Ou	itlet Devices
#1	Primary		" x 45.0' long Culvert CPP, square edge headwall, Ke= 0.500

Primary OutFlow Max=0.32 cfs @ 10.18 hrs HW=131.99' (Free Discharge)
1=Culvert (Barrel Controls 0.32 cfs @ 3.72 fps)

Pond 2P: 30" PIPE



WORKSHEET #3

DESIGN INFILTRATION RATE		
Kmeasured, Soil Infiltration Rate	11	5 IN/HR
Ft, Correction Factor for Testing	0.5	
Fp , Correction Factor for Plugging	0.0	
D, Depth to Water Table or Impervious Layer		FT.
W, Estimated Width of Facility		
Fg, Correction Factor for Geometry (0.25 min, 1.0 max.)	 	FT.
Kdesign, Design Infiltration Rate) INTO ID
Ruesign, Design militation Rate	0.6	IN/HR
BIORETENTION AREA NO. 1		
Total Proposed Impervious Area	7456	SF
Vdesign, One Inch Storm Volume	621	CU.FT.
L, Thickness of Planting Mix	24	IN.
D, Storage Depth Above Filter		IN.
Kdesign, Design Hydraulic Conductivity		IN/HR
T, Drawdown Time (Use 48 hrs)		HR.
Asf, Required Bioretention Area		SF
Asf, Proposed Bioretention Area		SF
Vactual, Volume Reduction Provided		CU. FT.
BIORETENTION AREA NO. 2		
Total Proposed Impervious Area	4700	SE.
Vdesign, One Inch Storm Volume		CU.FT.
L, Thickness of Planting Mix		IN.
D, Storage Depth Above Filter		IN.
Kdesign, Design Hydraulic Conductivity		IN/HR
T, Drawdown Time (Use 48 hrs)	*****	HR.
Asf, Required Bioretention Area	145	
Asf, Proposed Bioretention Area	558	
Vactual, Volume Reduction Provided		CU. FT.
BIORETENTION AREA NO. 3		
T-1-1-F		
Total Proposed Impervious Area	6472	
/design, One Inch Storm Volume		CU.FT.
, Thickness of Planting Mix		IN.
D, Storage Depth Above Filter		IN.
Kdesign, Design Hydraulic Conductivity		IN/HR
r, Drawdown Time (Use 48 hrs)		HR.
Asf, Required Bioretention Area	200	
Asf, Proposed Bioretention Area	255	
/actual, Volume Reduction Provided	689	CU. FT.
UMMARY		
otal Proposed Impervious Area	18628	SF
design, One Inch Storm Volume,		CU.FT.
actual, Volume Reduction Provided		CU. FT.
quivalent Impervious Area	34052	
otal Site Area	28350	